APPROPRIATENESS INVESTIGATION ON B60J68 AND A58N72 TURBOCHARGERS MATCHING FOR A COMMERCIAL VEHICLE

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Abstract
The manufacturers of the commercial vehicle adapts turbo charger for meeting the best performance at higher loads. The matching of perfect pair is tedious task and many methods are followed. As nowadays the turbochargers are supplier supplied products. This work adopts the simulation based matching and data-logger method for obtaining the operating conditions at various speeds. These obtained operating conditions were marked on the compressor map to find the best match. Objective of this work is to find appropriate turbocharger among B60J68 and A58N72 for the TATA 497 TCIC -BS III engine. The simulation results are validated with data-logger method by operated the vehicle at various routes namely Rough Road, Highway and slope up route at various engine speeds.
Index Terms: Turbo-charger, choke, surge, simulation, data-logger, turbo-matching.

I. INTRODUCTION

Turbo charger is an accessory in the IC engines to boost pressure, especially at higher loads. Turbo charger also helps to reduce specific fuel consumption (SFC), downsizing the engine, reduce CO_2 emission, etc.[1]-[5]. Due to the character of centrifugal compressor, the turbocharged engine yields lesser torque than naturally aspirated engine at lower speeds [6],[7]. Comparatively in diesel engine these problems very worse than petrol engine. Some of the system designs were made to mange this problem. They are: adopting the sequential system [8], incorporate the limiting fuel system, reducing the inertia, improvements on bearing, modification on aerodynamics [9], establishing electrically supported turbocharger [10], the usage of positive displacement charger i.e., secondary charging system and use of either electric compressor or positive displacement charger with turbocharger [10],[11] facilitating the geometrical variation on the compressor and turbine [12], adopting the twin turbo system [13], and dual stage system [14]. It is noticed that the transient condition is always worst with the engine which adopted single stage turbo charger. The variable geometry turbine was introduced for reducing the turbo lag in petrol as well as diesel engines. But the system is not exact match for petrol engines [15]. Even though many research were done on this case still the problem is exist. [12],[15]-[18]. Though the advancements in system design like variable geometry turbine, common rail injection system, and multiple injections, the problem is still persist due to the limiting parameter say supply of air. [19] discussed in detail about the benefits, limitations of turbo charger in single stage, parallel and series arrangements. According to the literature the turbocharger matching is a tedious job and demands enormous skill. The turbo matching can be defined as a task of selection of turbine and compressor for the specific brand of engine to meet its boosting requirements. That is, their combination to be optimized at full load. The trial and error method cannot be adopted in this case because the matching is directly effects as well as affects the engine performance [5],[20],[21]. So it is difficult task and to be worked out preciously. If one chooses the trial and error or non precious method, it will certainly lead to lower power output at low speeds for partly loaded engines for the case of two stage turbo charger. It is because of the availability of a very low pressure ratio after every stage than single stage [21]. Some cases the turbocharger characteristics are not readily available, and in some cases, not reliable or influenced by the engine which is to be matched [19]. Nowadays the Simulator is used for matching the turbocharger to the desired engine. The simulator was used to examine the performance at constant speed of 2000 rpm of two stage and single stage turbo chargers, the aim of the study was to optimize the high load limit in the Homogeneous charge compression ignition engine. For increasing the accuracy of matching the test bench method is evolved. Test bench was developed and turbo mapping constructed for various speeds to match the turbocharger for the IC engine by Leufven and Eriksson, but it is a drawn out process [21]. The on road test type investigation is called Data Logger based Matching method is adopted in this research. [22] discussed the data-logger turbocharger matching method in detail and compared with the result of test best method and simulator based matching method. And proved the data logger method outputs are reliable. By use of the data logger method the performance match can be evaluated with respect to various speeds as well as various road conditions. The core objective of this research is investigating the appropriateness of matching of the turbocharger with B60J68 and A58N72 for the TATA 497 TCIC -BS III Engine by simulator method. The validation of the same by Data Logger based Matching method.

II. MATERIALS AND METHODS

A logical science of combining the quality of turbocharger and engine and which is used to optimize the performance in specific operating range is called as turbo-matching. The Simulator method, data-logger method and Test Bed method is identified for this matching. Apart from the above three this research used the Simulator method and data-logger method for evaluating the performance of turbo matching. The trim size is a parameter, which can be obtained from the manufacture data directly or by simple calculation. That is the trim size is a ratio of diameters of the inducer to exducer in percentage. This parameter is closely related to the turbo matching. Various trim sizes are available, but in this study the trim size 68 and 72 are considered for investigation.

A. Simulator Based Matching

Various kinds of simulation software are being used for turbo matching. In this research the minimatch V10.5 software employed for turbo-matching by simulation. The manufacturer data of the engine and turbocharger are enough to find the matching performance by simulation. The manufacturer data are like turbo configuration, displacement, engine speed, boost pressure, inter cooler pressure drop and effectiveness, turbine and compressor efficiency, turbine expansion ratio etc. The software simulates and gives the particulars of the operating conditions like pressure ratio, mass flow rate, SFC, required power etc. at various speeds. These values are to be marked on the compressor map to know the matching performances. The compressor map is a plot which is used for matching the engine and turbocharger for better compressor efficiency by knowing the position of engine operating points. Based on the position of points and curve join those points the performance of matching will be decided.

B. Data Logger based Matching

This type of data collection and matching is like on road test of the vehicle. This setup is available in the vehicle with the provision of placing engine with turbocharger and connecting sensors. It is a real time field data gathering instrument called as Data-logger. It is a computer aided digital data recorder which records the operating condition of the engine and turbo during the road test. The inputs are gathered from various parts of engine and turbo charger by sensors. The Graphtec make data logger is employed in this work. It is a computerized monitoring of the various process parameters by means of sensors and sophisticated instruments. The captured data are stored in the system and plot the operating points on the compressor map (plot of pressure ratio versus mass flow rate). The Fig. 1 depicts the setup for the data-logger testing in which the turbocharger is highlighted with red circular mark.

C. *Decision Making*

The decision making process is based on the position of the operating points on the compressor map. The map has a curved region like an expanded hairpin, in which the left extreme region is called surge region. The operating points fall on the curve or beyond, is said to be occurrence of the surge. That means the mass flow rate limit below the compressor limit. This causes a risk of flow reversal. The right extreme region curve is called as Choke region. The points fall on the curve and beyond its right side is denoted as the occurrence of choke. In the choke region the upper mass flow limit above compressor capacity, which causes the quick fall of compressor efficiency, Chances for compressor end oil leakage and insufficient air supply. The all operating points fall in between those extreme regions i.e., the heart region holds good. It must be ensured at all levels of operation of the engine holds good with the turbocharger. The manufacturer of Turbocharger provides the compressor map for each turbo charger based on its specifications.

D. *Engine Specifications*

Table -1: Specification of Engine

Description	Specifications
Fuel Injection Pump	Electronic rotary type
Engine Rating	92 KW (125 PS)@2400 rpm
Torque	400 Nm @1300-1500rpm
No. of Cylinders	4 Cylinders in-line water cooled
Engine type	DI Diesel Engine
Engine Bore / Engine Stroke	97 mm/128mm.
Engine speed	2400 rpm (Max power), 1400 rpm (Max Torque)

The TATA 497 TCIC -BS III engine is a common rail type diesel engine. It is commonly used for medium type commercial vehicle like Tata Ultra 912 & Tata Ultra 812 trucks. The engine develops 123.29 BHP at 2,400 rpm and also develops the peak torque of 400 Nm between 1,300 and 1,800 rpm. The other specifications can be found in Table 1.

E. *Turbochargers Specifications*

The TATA Short Haulage Truck, turbochargers of B60J68 and A58N72 are considered to examine the performance of matching for TATA 497 TCIC -BS III engine. For example, if specification A58N72 means in which the A58 is the design code and N72 is the Trim Size of the turbocharger in percentage. The other specifications furnished in Table 2.

Table 2: Specification of Turbo Chargers

S.No	Description	B60J68	A58N72
1	Turbo max. Speed	200000 rpm	
2	Turbo Make	HOLSET	
3	Turbo Type	Waste gated Type with Intercooler	
4	Trim Size (%)	68	72
5	Inducer Diameter	46.9mm	50.1 mm
6	Exducer Diameter	68.9 mm	69.58 mm

III. EXPERIMENTAL OBSERVATION

The simulator and data-logger method is adopted to match the turbo Chargers B60J68 and A58N72 for TATA 497 TCIC -BS III engine. The matching performance can be obtained in the simulator by feeding necessary data from the manufacturer catalogue. The simulator simulates and presented the values of specific fuel consumption, pressure ratio and mass flow rate (Kg/sec.sqrt K/Mpa) at various speeds as measure of performances for identifying the matching performance of the turbo-charger for desired combination. The simulator based matching observations are obtained and presented as observation samples in the Table 3 and Table 4 for turbo Charger B60J68 and

A58N72 turbocharger respectively. In data-logger method the turbocharger is connected to the TATA 497 TCIC -BS III Engine of TATA 1109 TRUCK with sensors. The vehicle loaded to rated capacity 7.4 tonnes of net weight. The grass weight of vehicle is 11 tonnes. The experimental setup is shown in the Fig. I. The same operating speeds (1000, 1400, 1800 and 2400 rpm) were preferred to examine the matching performance on Highway, and slope up.

Figure 1 Experimental set up of Data-Logger method

Table-3: Simulated observations

S.N	Engine Speed	Mass Flow Rate		Pressure Ratio	
		B60J68	A58N72	B60J68	A58N72
1	1000	11.449	13.265	1.856	1.284
2	1400	22.56	24.789	3.051	2.678
3	1800	29.451	32.265	3.556	3.224
4	2400	36.872	36.256	3.817	3.427

Table- 4: Data-logger – Rough Road Route

S.N	Engine Speed	Mass Flow Rate		Pressure Ratio	
		B60J68	A58N72	B60J68	A58N72
1	1000	7.97	9.27	1.35	0.98
2	1400	15.79	17.12	1.95	1.73
3	1800	21.76	25.47	2.33	2.18
4	2400	27.41	29.59	2.60	2.34

Table- 5: Data-logger – Highway Route observations

S.N	Engine Speed	Mass Flow Rate		Pressure Ratio	
		B60J68	A58N72	B60J68	A58N72
1	1000	7.37	9.32	1.35	0.97
2	1400	15.41	17.23	1.95	1.77
3	1800	21.73	25.73	2.33	2.25
4	2400	27.43	29.72	2.55	2.38

Table- 6: Data-logger – City Drive observations

S.N	Engine Speed	Mass Flow Rate		Pressure Ratio	
		B60J68	A58N72	B60J68	A58N72
1	1000	7.41	9.43	7.41	0.99
2	1400	15.52	17.32	15.52	1.83
3	1800	21.68	25.84	21.68	2.29
4	2400	27.39	29.86	27.39	2.41

Table- 7: Data-logger – Slope Up observations

S.N	Engine Speed	Mass Flow Rate		Pressure Ratio	
		B60J68	A58N72	B60J68	A58N72
1	1000	8.12	9.39	1.35	0.97
2	1400	15.92	17.28	1.95	1.77
3	1800	21.87	25.79	2.33	2.25
4	2400	27.87	29.77	2.56	2.38

Table- 8 : Data-logger – Slope -Down observations

S.N	Engin e Speed	Mass Flow Rate		Pressure Ratio	
		B60J68	A58N7 2	B60J68	A58N72
1	1000	8.02	9.51	1.38	0.96
2	1400	15.81	17.76	2.00	1.85
3	1800	21.94	25.95	2.39	2.3
4	2400	27.97	29.93	2.62	2.46

IV. RESULTS AND DISCUSSIONS

The turbo-match observations were obtained for both turbo-chargers with engine in both simulation and data-logger method with rough road route, highway route and slop-up route. Those observations were road condition wise with simulated observations plotted on the respective compressor map. The details of such maps are: the Fig.2 and Fig.3 are for simulation and data-logger Rough route observations for turbo-matching of turbo chargers B60J68 and A58N72 respectively. Similarly Fig.4 and Fig.5 for Highway route, Fig.6 and Fig.7 for City Drive route, Fig.8 and Fig.9 for Slope up and Fig.10 and Fig.11 for Slope down.

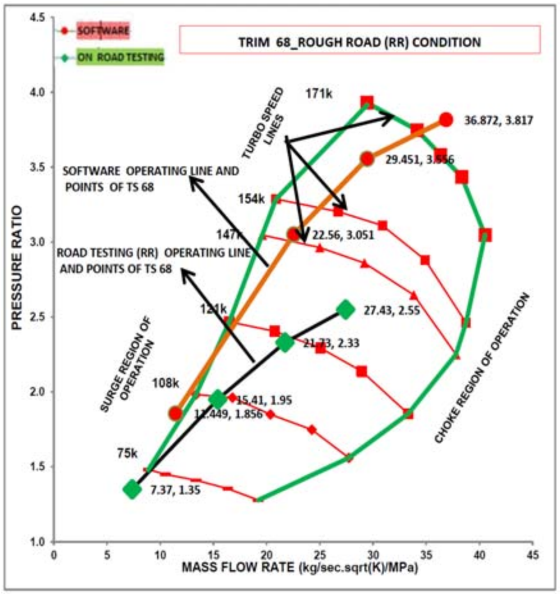

Fig. 2 B60J68 Turbo-match-Rough Road

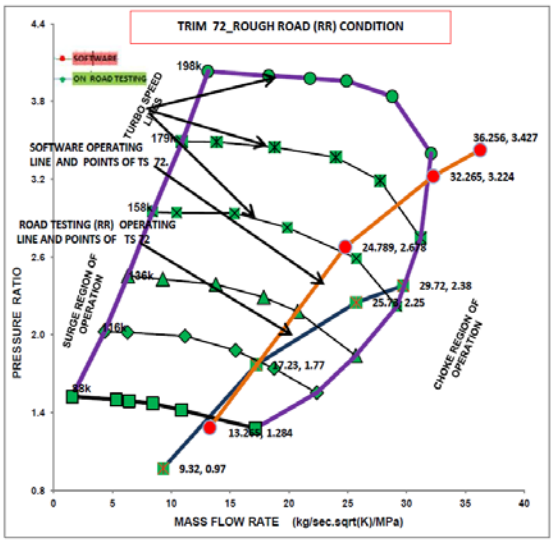

Fig. 3 A58N72 Turbo-match-Rough Road

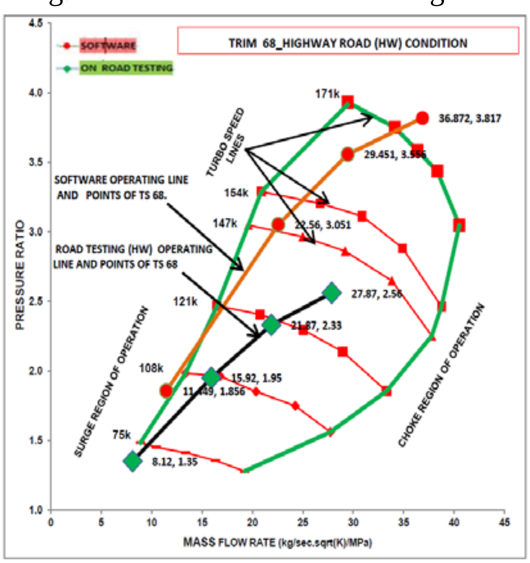

Fig. 4 B60J68 Turbo-match-Highway Road

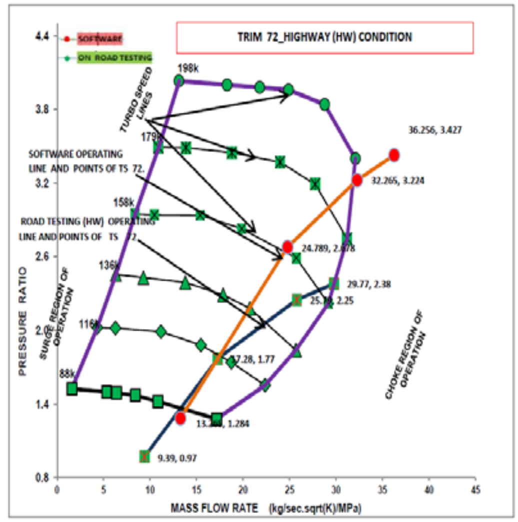

Fig. 5 A58N72 Turbo-match – Highway

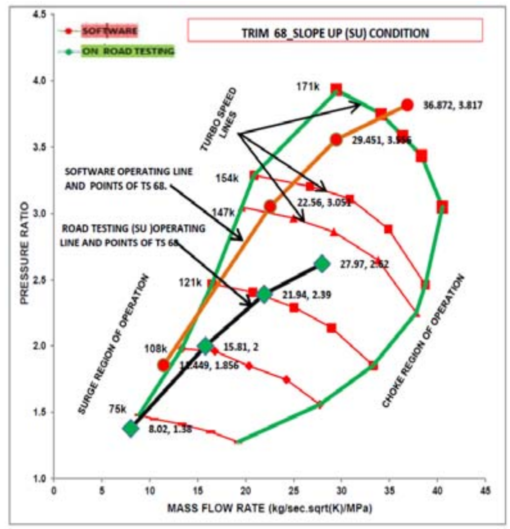

Fig. 6 B60J68 Turbo-match- Slope-up

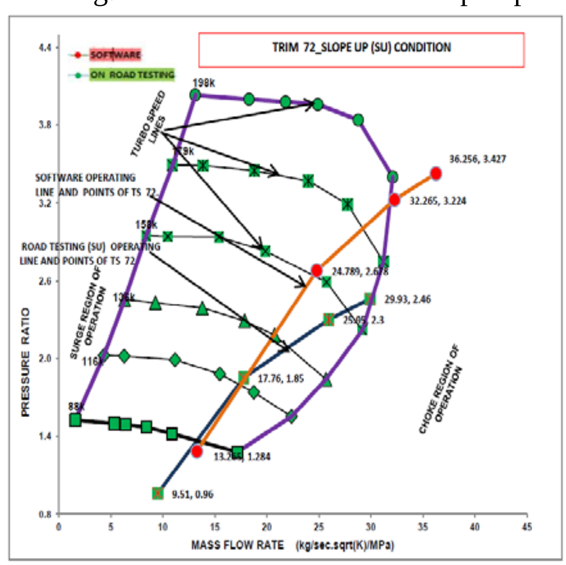

Fig. 7 A58N72 Turbo-match – Slope up

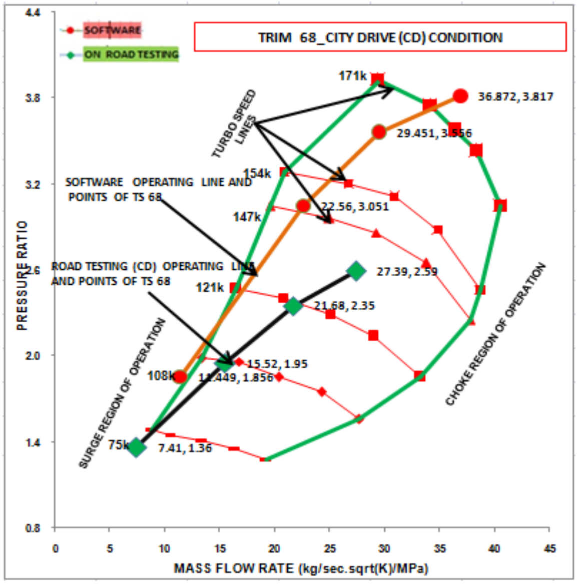

Fig. 8 B60J68 Turbo-match- City Drive

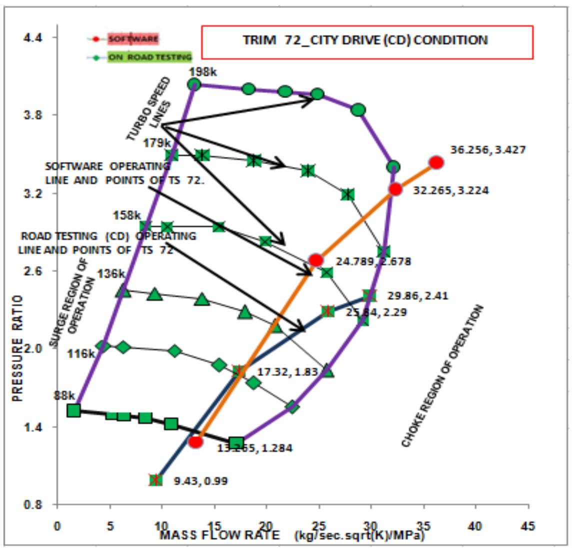

Fig. 9 A58N72 Turbo-match – City Drive

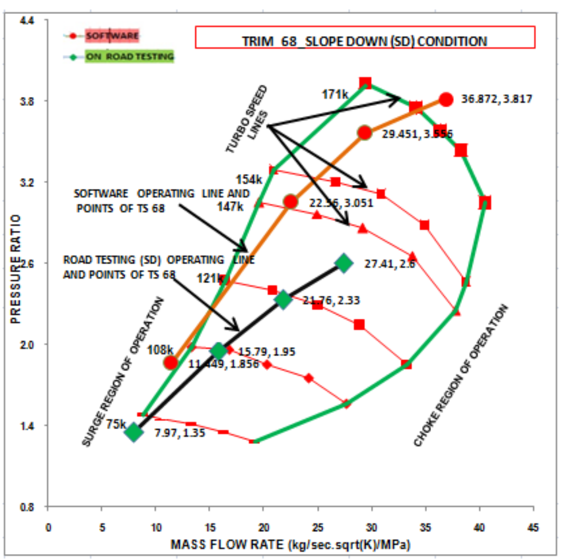

Fig. 10 B60J68 Turbo-match- Slope Down

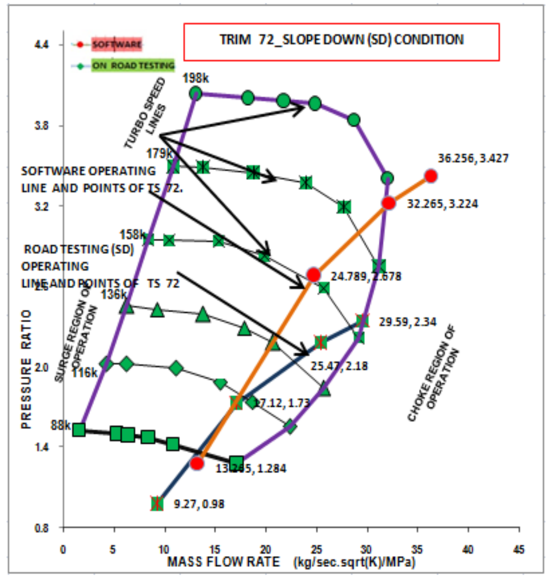

Fig. 11 A58N72 Turbo-match – Slope Down

It was observed from the compressor maps (figure 2 to Figure 11) that the simulated values are slightly higher than the data-logger observation values. But according to the data logger, the turbo-match of B60J68 turbo-charger gives safe performance at all speed range. At lower engine speed (1000 rpm), the surge may be occurred, because such operating conditions are near by the surge line. The minimum speed may be slightly increased for safe performance. The engine combination with A58N72 Turbo-charger, offers good operating performance of operating at lower and medium engine speeds, but at higher speeds (2400 rpm) choke occurs. Because the operating conditions found on the line of choke in the compressor map. This may be compensated by sightly reduce the maximum speed of the engine.

V. CONCLUSION

The appropriateness of turbo-matching of B60J68 turbocharger and A58N72 turbocharger for TATA 497 TCIC -BS III engine is discussed in this paper. The simulation and data-logger methods adapted for the evaluation. The simulation values higher than the data-logger values in all preferred routes of operation of vehicle. In the evaluation B60J68 turbo-match requires increase of minimum speed from 1000 rpm, on other hand A58N72 turbo match requires reduction of maximum engine speed from 2400 rpm. Hence it is concluded that both the turbo-chargers can be matched to TATA 497 TCIC -BS III engine with the condition of alteration of limits of engine speed (either maximum or minimum) should not affects significantly the vehicle performance and cost of operation etc. The data-logger method adapted in this research may feel as expensive but it is one time job of finding the best turbo-match for an engine category.

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